

# FABRIC PERMEABILITY TESTING AND THEIR USE IN INFUSION SIMULATION

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### Infusion process

RTM – Resin Transfer Molding  
VARI – Vacuum Assisted Resin Infusion

Darcy's law:  
$$v = -\frac{1}{\phi\mu} K \cdot \nabla P$$

Continuity equation:  
$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho v) = 0$$

**RTM**

2D infusion  
 $V_f = \text{const.}$

$$K = \begin{bmatrix} k_1 & 0 \\ 0 & k_2 \end{bmatrix} = \text{const.}$$

**VARI (no flow media)**

2D infusion  
 $V_f \neq \text{const.}$

$$K(V_f) = \begin{bmatrix} k_1(V_f) & 0 \\ 0 & k_2(V_f) \end{bmatrix}$$

**VARI (with flow media)**

3D infusion  
 $V_f \neq \text{const.}$

$K = f(V_f, t, P)$   
 $P = P_{\text{resin}} + P_{\text{preform}}$

$$K(V_f) = \begin{bmatrix} k_1(V_f) & 0 & 0 \\ \text{sym} & k_2(V_f) & 0 \\ & & k_3(V_f) \end{bmatrix}$$

Figures adapted from 1

### Permeability testing

was performed on the *fabric* (quasi UD), *flow media* and several stacks' *interfaces*, namely *foam-fabric* and *flow media-fabric* (effective permeability of the corresponding interface is reduced due to nesting). Through-thickness fabric permeability was estimated via one point infusion test<sup>2</sup> and simulation fitting<sup>3</sup> (resin used was RIMR235-H237).

**Foam-fabric interface**

$P = 0.1 \text{ MPa}$

$7.1\text{E-}11$   $3.7\text{E-}11$   $2.3\text{E-}11$

**Flow media-fabric interface**

$P = 0.1 \text{ MPa}$

$8.0\text{E-}10$   $3.5\text{E-}10$   $4.1\text{E-}10$

**Fabric through-thickness**

$P = 0 \dots 0.1 \text{ MPa}$

$5.0\text{E-}13$

$K_x, \text{m}^2$

### Demonstration module

consists of four C-Spars molded to an outer skin. The central portion of the panel uses a sandwich construction filled with foam core.

### Simulation models

represents a quarter of module, with separate FE layers for each fabric ply (~700 000 elements).

- Flow media on all surfaces
- Flow media area reduced

### Tests and simulations results comparison

- Flow media on all surfaces
 

17 sec  
  
18 sec

241 sec  
  
237 sec

311 sec  
  
317 sec
- Flow media area is reduced
 

16 sec  
  
19 sec

470 sec  
  
1845 sec\*\*

875 sec  
  
2502 sec\*\*

Filling defects

Cured module

PAM-RTM™ software<sup>3</sup> was used for simulations.  
\*\* - pronounced disagreement between test and simulation filling times is due to VARI specific phenomena (e.g. thickness and permeability variation) which are not taken into account in the current simulation model

### Conclusions

- boundary interface effects have to be taken into account
- changing pressure results in variable preform thickness ( $V_f$ ) and permeability
- for accurate simulation the above effects have to be accounted for

### Future work

- 2D and 3D simulation with permeability and fiber volume fraction as a function of pressure

### Preform thickness change during VARI process

(GOM-Aramis optical measurements system)

\* - 'Simulation based solutions for industrial manufacture of large infusion composite parts' - A CEC Framework VII collaborative research project to develop new technologies and simulation tools to predict Liquid Resin Infusion (LRI) of large aircraft composite structures (Coordinator: Anthony Pickett (ESI GmbH, Germany)).  
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